

## Metal Matrix Composites for Ordnance Applications

Christopher Hoppel, Ph.D.
John H. Beatty, Ph.D.
Jonathan S. Montgomery, Ph.D.
James M. Bender
Travis A. Bogetti, Ph.D.

U.S. Army Research Laboratory Aberdeen Proving Ground, MD 21005

NDIA Firepower Symposium 20 June 2001



## Metal Matrix Composites for Ordnance Applications Outline



- Motivation
- Background
  - → Army History
  - → 3M DARPA Program
- Development of Analysis Methodology
  - → Lamina or Ply Level
  - → Laminate Level
- Application Projectile Shell
- Conclusions



#### **Motivation**



**Outstanding Mechanical and Thermal Properties** 

Specific fiber direction stiffness comparable to carbon/epoxy

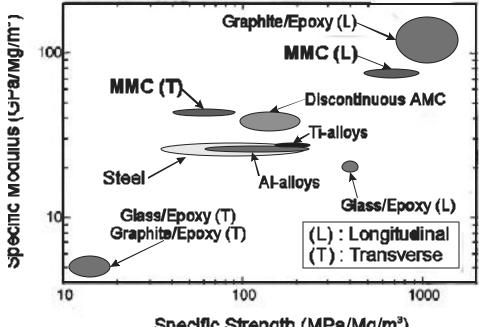
Transverse and shear properties much greater than

carbon/epoxy

 Very high compression strength (~500 ksi)



- High thermal conduction (~5 times graphite/epoxy)
- Low CTE
- High melting point



Specific Strength (MPa/Mg/m³)

#### Objective Force has Critical Need for Lightweight, High **Performance Materials**

- Optimized Projectiles
- Lightweight Gun Tubes







- Metal Matrix Composites have drawn strong interest from the Army for over 30 years
  - AMMRC, MTL, BRL, and ARL have funded research since 1960's
  - Over 60 reports in this area

#### **■** Diverse applications have been investigated

- Tank track shoes
- Helicopter transmission casings, landing gears, skids and wear pads
- Ballistic missile structural components
- Lightweight assault bridging components
- .50 caliber machine gun components

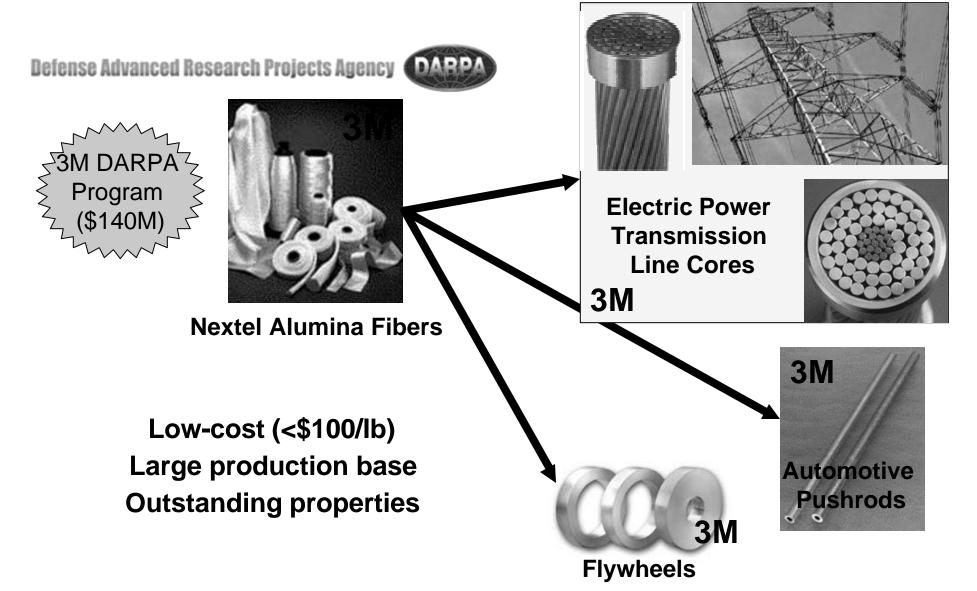
#### ■ Widespread use has been limited by

- High material costs
- Lack of a reasonable production base
- Lack of design tools



#### **3M Production Base**







#### Metal Matrix Composites for Ordnance Applications (STO IV.MA.2001.01)



Objective: Develop metal matrix composite technology for more lethal projectiles and lighter armaments for FCS





#### **Pacing Technologies:**

- Artillery Projectile:
  - $\rightarrow$  Joining Technology
  - $\rightarrow$  Processing
- Gun Barrel:
  - → Thermal Fatigue
  - $\rightarrow$  Processing

#### **Warfighter Payoffs:**

- Enhanced Lethality and Survivability
- Lightweight projectiles with greater payload capacity
- Lightweight armament systems

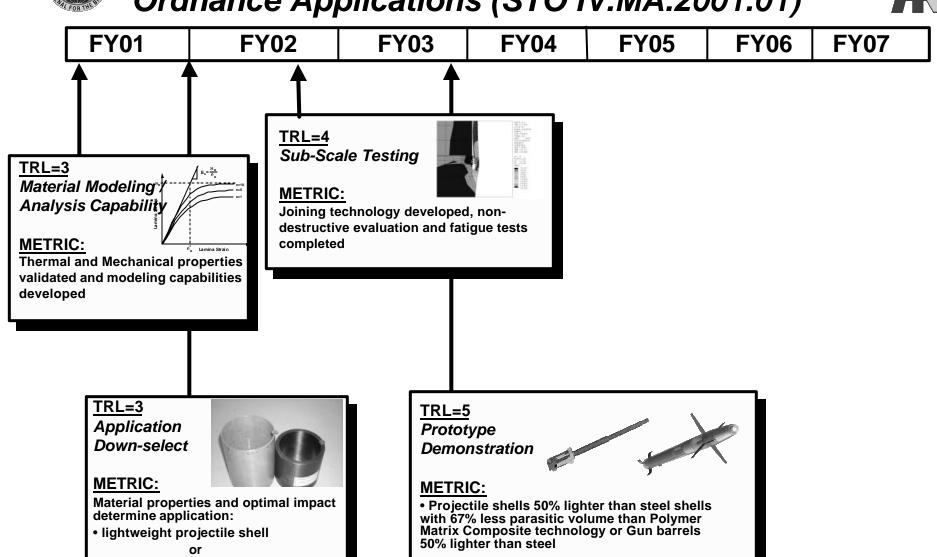
Projectile shells 50% lighter than steel shells with 67% less parasitic volume than polymer matrix composite shells; Gun barrels 50% lighter than steel



lightweight barrel component

#### Metal Matrix Composites for Ordnance Applications (STO IV.MA.2001.01)





Ammunition ATD

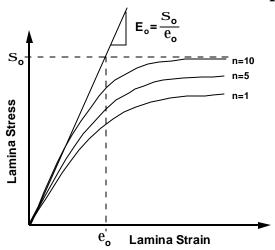
Transition to Multi-Role Armament &

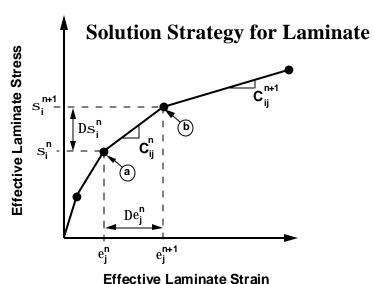


#### Nonlinear Composite Modeling - Approach

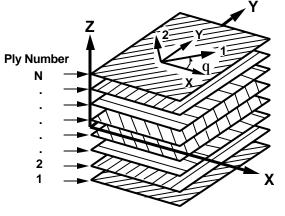


#### **Characterize Lamina Level Properties**

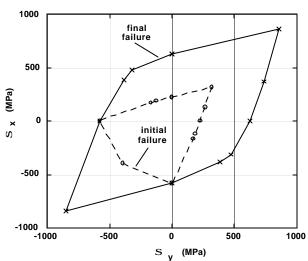




#### **Allow for Arbitrary Lay-Ups**



#### **Failure Prediction for Multi-Axial Loading**





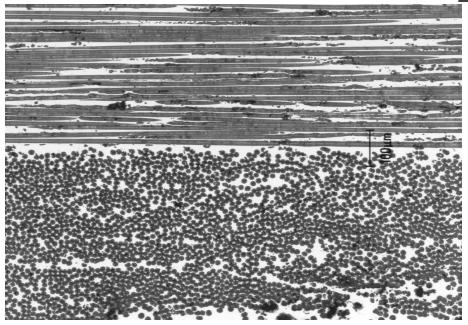
#### **Composite Mechanics**

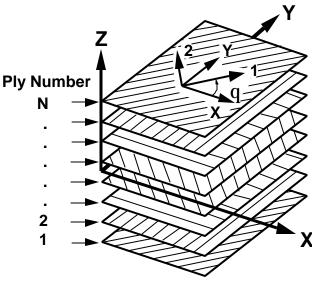
#### **■** Lamina or Ply Properties

- -Individual ply or layer
- –Properties dominated by
  - » Fiber
  - » Matrix
  - » Interface
- -Nine failure modes

#### **■** Laminate Properties

- -Series of lamina
- -Properties dominated by
  - » Lamina properties
  - » Order and Orientation of lamina







#### **Lamina Properties**



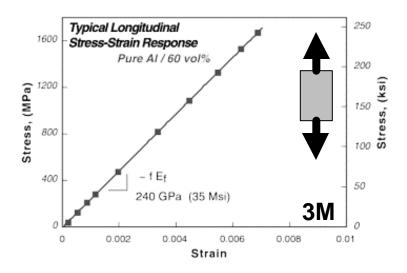
#### **■** Tensile Properties

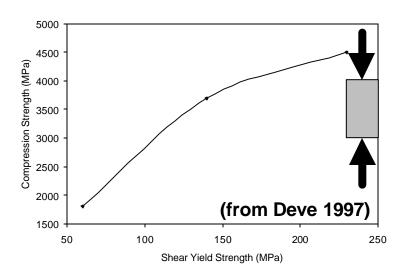
- –Dominated by fibers
- -Strength and Stiffness are linearly proportional to the fiber volume fraction

#### **■** Compression properties

- Stiffness is proportional to fiber volume fraction
- Strength is dominated by shear yield strength of matrix

$$\mathbf{S}_{c} = \mathbf{G}_{\hat{\mathbf{e}}}^{\hat{\mathbf{e}}} \mathbf{1} + \mathbf{n}_{\hat{\mathbf{c}}}^{\mathbf{z}} \mathbf{3}_{\hat{\mathbf{o}}}^{\mathbf{n}} \mathbf{x}^{\mathbf{z}} \mathbf{F} \mathbf{F}_{\hat{\mathbf{e}}}^{\mathbf{z}} \mathbf{0}^{\mathbf{n}-\frac{1}{n}} \mathbf{u}^{\mathbf{z}-1} \mathbf{x}^{\mathbf{z}} \mathbf{x}^{\mathbf{z}} \mathbf{F}_{\hat{\mathbf{e}}}^{\mathbf{z}} \mathbf{0}^{\mathbf{z}} \mathbf{x}^{\mathbf{z}} \mathbf{$$







## Transverse and Shear Lamina Properties

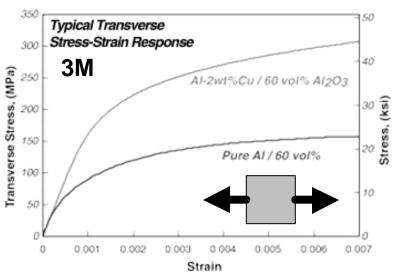


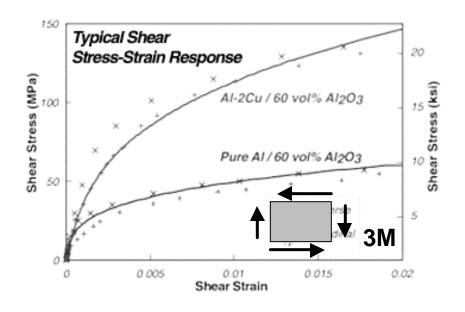
#### ■ Stress-Strain Response

Initial modulus defined by rule-of-mixtures

$$\frac{1}{E_c} = \frac{V_f}{E_f} + \frac{V_m}{E_m}$$

- Overall response is nonlinear and dependent on matrix
- Transverse and shear properties more important in MMCs than PMCs
  - For MMC  $E_T = 138$  GPa
  - For PMC  $E_T = 7$  GPa







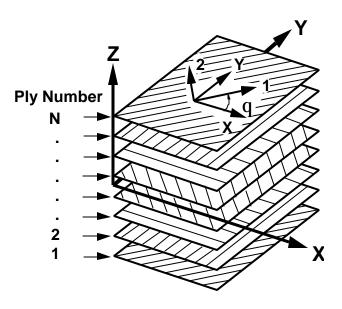
#### Laminate Mechanics



- Classical laminate mechanics can be used to accurately predict the initial linear-elastic behavior of MMC laminates
- More advanced methodologies are needed to predict full stress-strain curve
  - Non-linear shear and transverse properties
  - Progressive failure of lamina

Predicted and Observed Strength and Modulus for  $\pm$  22.5 FP-alumina/Mg

Property	Temperature °F	Calculated	Measured
Ex	70	24.5Msi	27.7Msi
Ey	70	15.3Msi	13.82
σL	70	74 ksi	66
$\sigma$ T	70	35.2ksi	35.2
Ex	300	23.9Msi	23.2
Ey	300	13.95	13.53
۵۲	300	74	59.6
στ	300	35.2	31.9



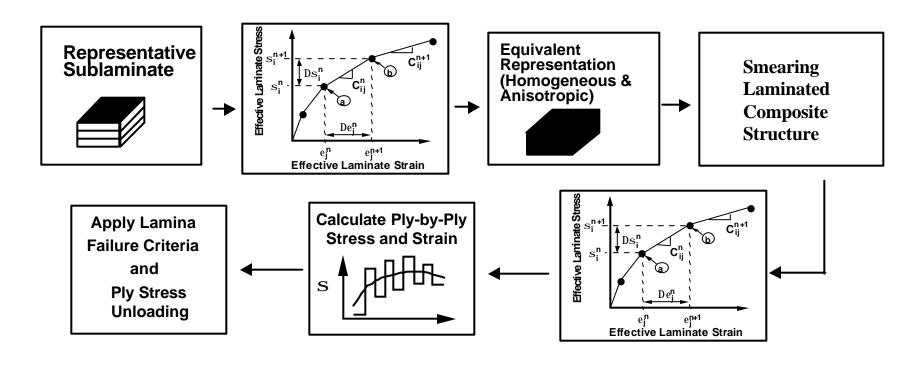


# Non-linear Progressive Laminate Analysis



#### **Approach**

- Piecewise Linear Increments
- Superimposed to Form Effective Nonlinear Response
- Individual Ply Stress, Strain and Stiffness
- Ply Stress or Strain Allowables
- FEA for Structure

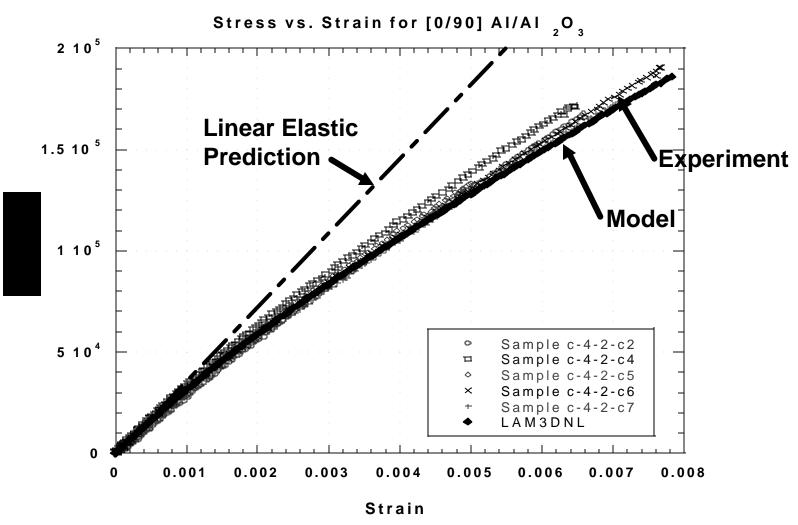






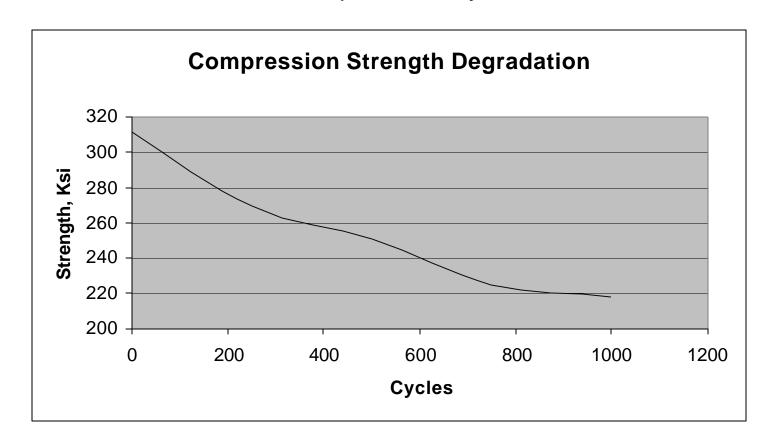


Compressive stress-strain response of Al with 65%  $Al_2O_3$  fibers with a  $[0/90]_{4S}$  architecture



#### **Thermal Fatigue Testing**

- Testing done by LTC John Bridge at USMA
  - Specimens from 3M's automotive pushrods (commercial product)
  - Cycled at 300°C
  - Loss of 30% of compression strength after 1000 cycles
  - Matrix was Al-2wt%Cu, pure Al may behave better

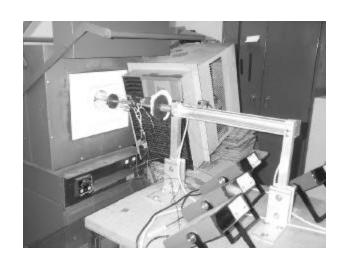




#### **Experimental Procedures**



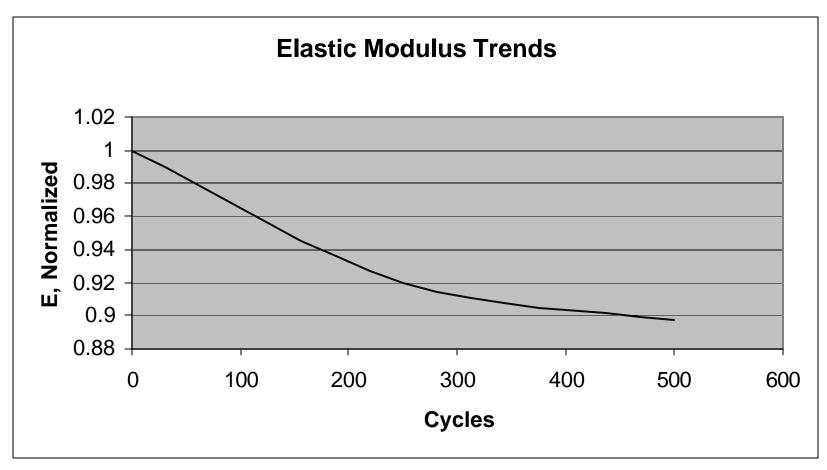
- Specimens: 6 inch Long Hollow Rods 0.375 in. Wall Thickness
- **■** Electro-Pneumatic Piston Cycling Device
  - Timer, Solenoids, Air Compressor, Counter, Air-Conditioner, Thermocouples, Fans
- Specimen "Cage"
- Insulated Convection Furnace
- 0 to 300 Degree C Thermal Range
- 2.5 Minute Cycle Time
- **250 Cycle Intervals up to 1000 Cycles**
- Specimens Tested at each 250 Cycle Interval





#### **Compression Tests - Elastic**







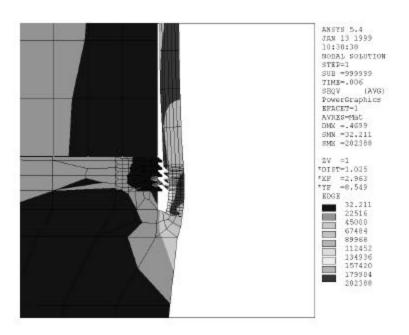
# Lightweight Ordnance Metal Matrix Composites for Ordnance Applications



### SADARM carrying variant of the XM982 projectile

- Exhibits excessive deformation under setback loading
- Steel shell exceeds weight goal
- Space constraints limit redesign options
- MMC shell necessary for projectile







#### Material Impact: Artillery Shell



# Comparison of an 18-in 155-mm Artillery Shell made from Steel, Aluminum Metal Matrix Composites, and Graphite/Epoxy.

	Shell	Weight	Available	Internal Vol.
Material	Weight	Normalized	Volume	Normalized
	(lbs)	to Steel	$(in^3)$	to Steel
Steel	11.95	1.00	484	1.00
AMC [0/90]	5.15	0.43	484	1.00
AS4/3501	7.10	0.59	400	0.83
[0/90]				

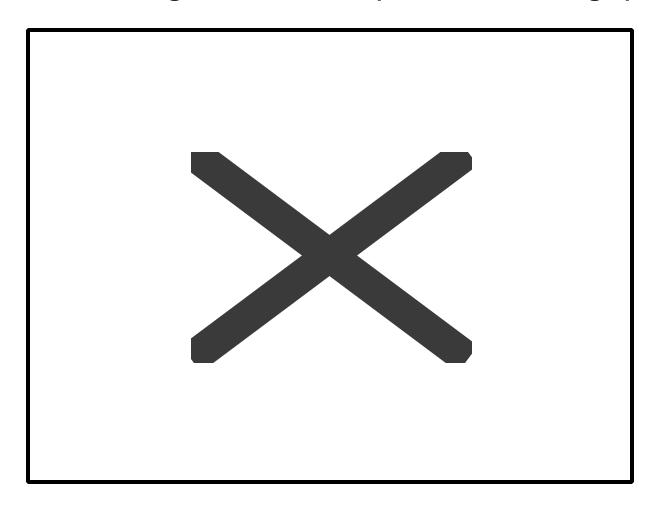




## MMC 155-mm Shell Crush Test Results



Failure Strength, 483,000 lbs (25 lbs @ 19,300 g's)





#### **Conclusions**



- Metal Matrix Composites have outstanding potential for Ordnance
  - Projectile shells 50% lighter than steel, with 67% less parasitic volume than polymer matrix composites
  - Gun barrels 50% lighter than steel
- Modeling technologies developed to allow design for ordnance applications
  - Lamina-level
  - Gun barrel and Projectile shell components
- STO Program will demonstrate technology for Objective Force
  - Develop Prototype of gun barrel or projectile shell
  - TRL 5 by 2003